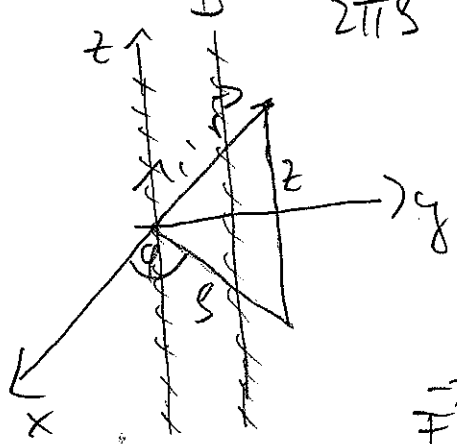


# Problems Chapter 10.

(1) The first wire produces the  $\vec{B}$  field

$$\vec{B} = \frac{\mu_0 i \vec{e}_\phi}{2\pi R}$$



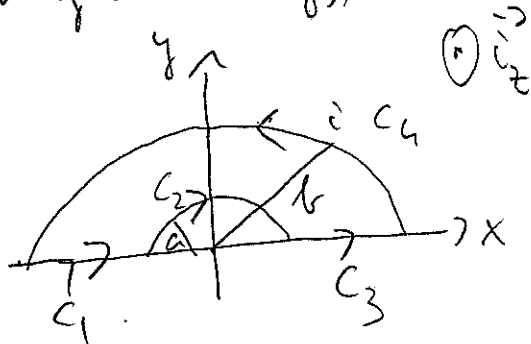
$S: \phi, z$ : usual cylindrical coordinates

The second wire may be at  $S = a$  carrying current  $i'$ : A piece of length  $l$  lies flat the base

$$\begin{aligned} \vec{F} &= \frac{\mu_0 i \vec{e}_\phi}{2\pi a} \times i' l \vec{e}_z \\ &= -\frac{\mu_0 i i' l}{2\pi a} \vec{e}_\phi \end{aligned}$$

Thus if the currents go in the same (opposite) direction the force is attractive (repulsive) the wires to each other.

(2)



Parameterizations:

$$C_1: \vec{r}^1 = x \vec{e}_x; x \in (-b, -a) \Rightarrow d\vec{r}^1 = dx \vec{e}_x$$

$$C_2: \vec{r}^1 = (a \vec{e}_\phi) \vec{e}_\phi; \phi \text{ from } \pi \rightarrow 0 \Rightarrow d\vec{r}^1 = a d\phi \vec{e}_\phi$$

$$C_3: \vec{r}^1 = x \vec{e}_x; x \in (a, b) \Rightarrow d\vec{r}^1 = dx \vec{e}_x$$

$$C_4: \vec{r}^1 = b \vec{e}_\phi(\phi); \phi \in (0, \pi) \Rightarrow d\vec{r}^1 = b d\phi \vec{e}_\phi$$

$$\vec{B}(\vec{r}=0) = \int_{C_1+C_2+C_3+C_4} d\vec{r}' \times \frac{\mu_0 i}{4\pi} \frac{-\vec{r}'}{r'^3}$$

The lines  $C_1$  and  $C_3$  do not contribute since  $d\vec{r}' \times \vec{r}' = 0$

$$\Rightarrow \vec{B}_2(\vec{r}=0) = \int_0^\pi d\varphi a \vec{i}_\varphi \times \frac{\mu_0 i}{4\pi} \frac{(-\vec{i}_\varphi(a))}{a^2} = -\frac{\mu_0 i}{4a} \vec{i}_z$$

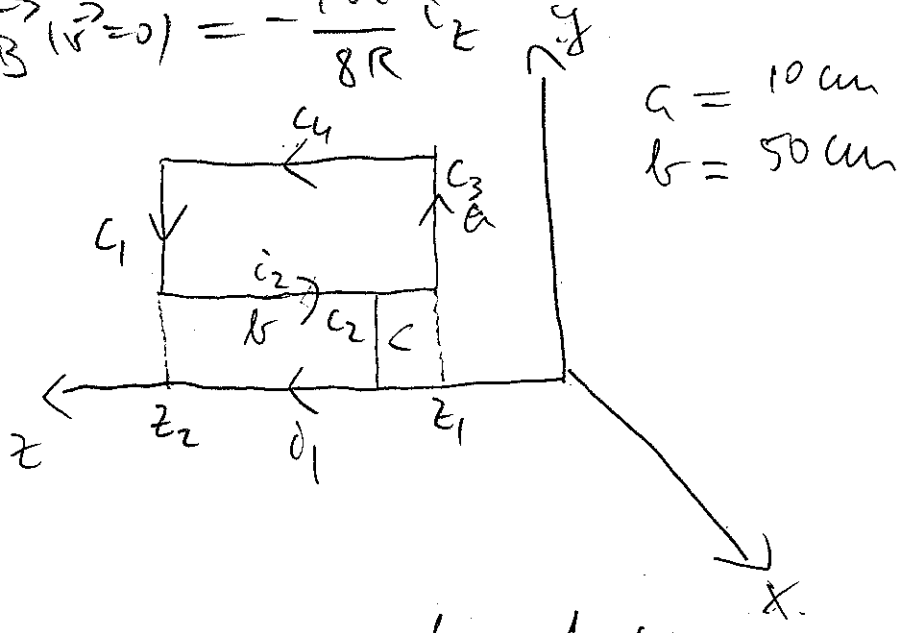
$$\vec{B}_4(\vec{r}=0) = \int_0^\pi d\varphi b \vec{i}_\varphi \times \frac{\mu_0 i}{4\pi} \frac{(-\vec{i}_\varphi(b))}{b^2} = \frac{\mu_0 i}{4b} \vec{i}_z$$

$$\Rightarrow \vec{B}(\vec{r}=0) = -\frac{\mu_0 i}{4} \left(\frac{1}{a} - \frac{1}{b}\right) \vec{i}_z$$

For  $a=R$  and  $b=2R$

$$\vec{B}(\vec{r}=0) = -\frac{\mu_0 i}{8R} \vec{i}_z$$

(3)



In the  $xy$  plane we have  $xy > 0$

$$\vec{B} = -\frac{\mu_0 i}{2\pi xy} \vec{i}_x \quad \left( \text{Since } \vec{i}_\varphi(\varphi = \frac{\pi}{2}) = -\vec{i}_x \right)$$

Forces on  $C_1$  and  $C_4$  with  $y$  running from  $a+c$  to  $c$

$$C_1: \vec{r} = y \vec{i}_y + z_2 \vec{i}_z$$

$$\vec{F}_1 = \int_{a+c}^c dy \vec{i}_y \times (-z_2 \vec{i}_y) \vec{i}_z \times \left( -\frac{\mu_0 i}{2\pi xy} \vec{i}_x \right)$$

$$\vec{F}_1 = \vec{i}_z \frac{\mu_0 i_2 I_0}{2\pi r} \int_{a+c}^c dy \frac{1}{y} = \frac{\mu_0 i_2}{2\pi I_0} \ln\left(\frac{c}{a+c}\right) \vec{i}_z \quad (3)$$

$$= -\frac{\mu_0 i_2 I_0}{2\pi} \ln\left(\frac{a+c}{c}\right) \vec{i}_z$$

Since for  $C_3$  we have the same integral in the opposite direction, because  $\vec{B}$  does not depend on  $z$ ,  $\vec{F}_3 = -\vec{F}_1$ .

$$C_2: \vec{F}_2 = -\mu_0 i_2 \vec{i}_z \times \left(-\frac{\mu_0 i_1}{2\pi c} \vec{i}_x\right)$$

$$= \frac{\mu_0 i_1 i_2 b}{2\pi c} \vec{i}_y$$

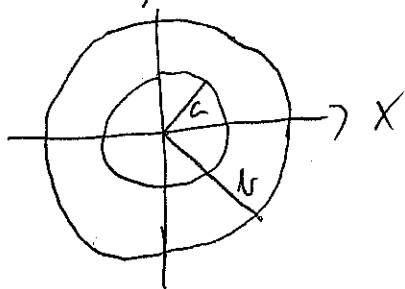
$$C_4: \vec{F}_4 = -\frac{\mu_0 i_1 i_2 b}{2\pi (a+c)} \vec{i}_y$$

$$\Rightarrow \vec{F}_{\text{total}} = \frac{\mu_0 i_1 i_2 b}{2\pi} \left(\frac{1}{c} - \frac{1}{a+c}\right) \vec{i}_y = 10^{-5} \text{ N } \vec{i}_y$$

(4) See behavior

(5) — " —  $Oz$

(6)



$$\vec{j} = \begin{cases} \frac{i}{\pi (b^2 - a^2)} \vec{i}_z & \text{for } a < \rho < b \\ 0 & \text{elsewhere} \end{cases} \Rightarrow \vec{B} = B_\varphi \vec{i}_\varphi$$

Ampere's law with circles of radius  $S$ :

$$\oint_C d\vec{r} \cdot \vec{B} = 2\pi S \cdot B_\varphi = \mu_0 i_{\text{enclosed}}$$

$$\Rightarrow B_\phi = 0 \text{ for } 0 < s < a$$

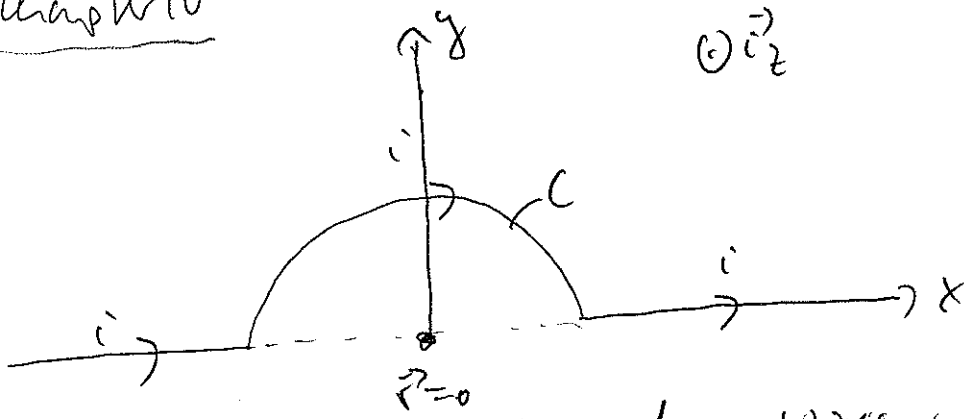
$$B_\phi = \frac{\mu_0 i}{2\pi s} \frac{\pi (b^2 - a^2)}{\pi (b^2 - a^2)} = \frac{\mu_0 i}{2\pi s} \frac{b^2 - a^2}{b^2 - a^2} \text{ for } a < s < b$$

$$B_\phi = \frac{\mu_0 i}{2\pi s} \text{ for } s > b$$

(9)

Exercises Chapter 10

(1)

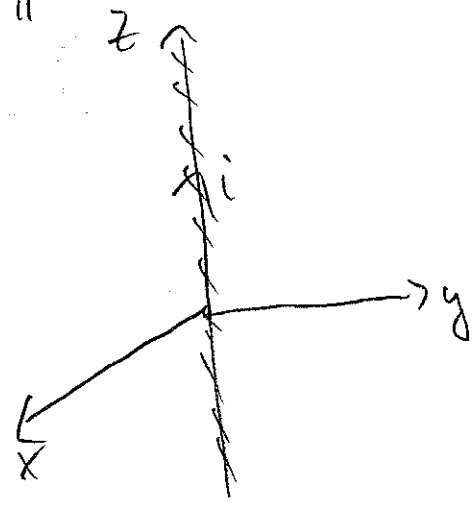


Biot-Savart law  $\Rightarrow$  no contribution from wires along x axis.  $i \hat{z}$   
 For semi circle:

$C: \vec{r}' = R \hat{e}_\rho(\phi)$  with  $\phi$  from  $\pi \rightarrow 0$ ;  $d\vec{r}' = R \hat{e}_\phi(\phi)$

$$\vec{B} = \frac{\mu_0 i}{4\pi} \int_{\pi}^0 d\phi R \hat{e}_\phi(\phi) \times \frac{-R \hat{z}(\phi)}{R^2} = -\frac{\mu_0 i}{4R} \hat{z}$$

(2)



$$\vec{B} = \frac{\mu_0 i}{2\pi s} \hat{e}_\phi$$

$$\vec{F} = q \vec{v}_0 \times \vec{B}$$

(a)  $\vec{v}_0 = v_0 \hat{z} \Rightarrow \vec{F} = \frac{q \mu_0 i v_0}{2\pi d} (-\hat{e}_\phi)$

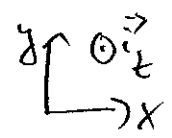
(b)  $\vec{v}_0 = v_0 \hat{y} \Rightarrow \vec{F} = \frac{q \mu_0 i v_0}{2\pi d} \hat{z}$

(c)  $\vec{v}_0 = v_0 \hat{e}_\phi \Rightarrow \vec{F} = 0$

(3) Let  $\vec{i}_z$  come out of the plane. Then at the center wire:

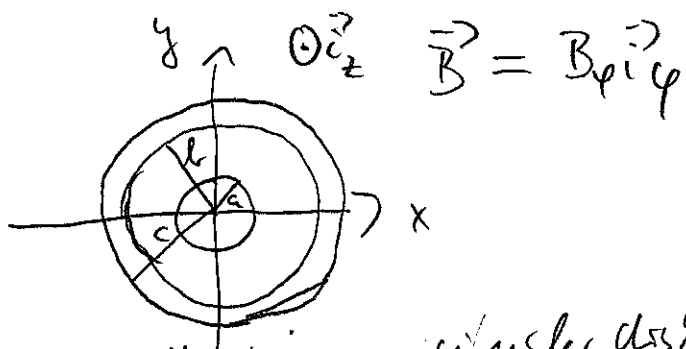
(2)

$$\vec{B} = \vec{B}_1 + \vec{B}_2 = \frac{\mu_0}{2\pi} \left( -\frac{i_1}{l_1} + \frac{i_3}{l_2} \right) \vec{i}_z$$

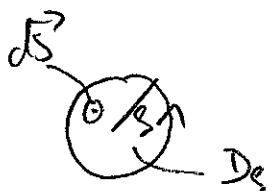


$$\vec{F} = i_2 l \vec{i}_x \times \vec{B} = \frac{\mu_0 i_2 l}{2\pi} \left( \frac{i_1}{l_1} - \frac{i_3}{l_2} \right) \vec{i}_y$$

(4)



Ampere's law with wire = circular disk of radius  $s$



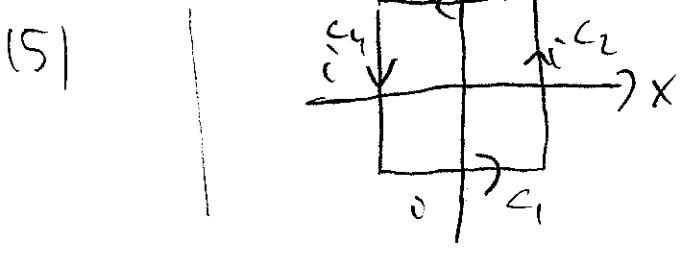
$$\vec{J} = \begin{cases} -\frac{i}{\pi a^2} \vec{i}_z & \text{for } 0 < s < a \\ +\frac{i}{\pi(c^2 - b^2)} \vec{i}_z & \text{for } b < s < c \\ 0 & \text{elsewhere} \end{cases}$$

$$\oint_{\partial D_s} d\vec{r} \cdot \vec{B} = \int_{D_s} d\vec{S} \cdot \vec{J}$$

$$2\pi s B_\phi = \mu_0 i \text{ inside} = \mu_0 \begin{cases} -\frac{i\pi s^2}{\pi a^2} & \text{for } 0 < s < a \\ -i & \text{for } a < s < b \\ -i + \frac{i\pi(s^2 - b^2)}{\pi(c^2 - b^2)} & \text{for } b < s < c \\ 0 & \text{for } s > c \end{cases}$$

$$\frac{B}{\mu_0 i} = \begin{cases} -s^2/a^2 & \text{for } 0 < s < a \\ -1 & \text{for } a < s < b \\ -\frac{c^2-s^2}{c^2-b^2} & \text{for } b < s < c \\ 0 & \text{for } s > c \end{cases}$$

B is always tangential to the circles in clockwise direction!



Biot-Savart Law

$$C_1: \vec{r} = -\frac{l}{2} \vec{e}_y + x \vec{e}_x \quad ; x \in (-\frac{l}{2}, \frac{l}{2})$$

$$\vec{B} = \frac{\mu_0 i}{4\pi} \int_{-l/2}^{l/2} dx \vec{e}_x \times \frac{l}{2} \vec{e}_y \frac{1}{(x^2 + \frac{l^2}{4})^{3/2}}$$

$$= \frac{\mu_0 i}{4\pi} \frac{l}{2} \int_{-l/2}^{l/2} dx \frac{\vec{e}_z}{(x^2 + \frac{l^2}{4})^{3/2}} = \frac{\mu_0 i l}{4\pi} \int_0^{l/2} dx \frac{\vec{e}_z}{(x^2 + \frac{l^2}{4})^{3/2}}$$

$$\int dx \frac{1}{(x^2 + a^2)^{3/2}} = \int ds a \cosh u \frac{1}{a^3 \cosh^3 u} = \frac{1}{a^2} \int ds \frac{1}{\cosh^2 u} = \frac{\tanh u}{a^2}$$

$$x = a \sinh u \Rightarrow dx = a \cosh u \, du$$

$$a = \frac{l}{2} \Rightarrow x = a \Rightarrow \sinh u = 1 \Rightarrow \tanh u = \frac{1}{\sqrt{2}} = \frac{\sqrt{2}}{2}$$

$$\Rightarrow x = 0 \Rightarrow \sinh u = 0 \Rightarrow \tanh u = 0$$

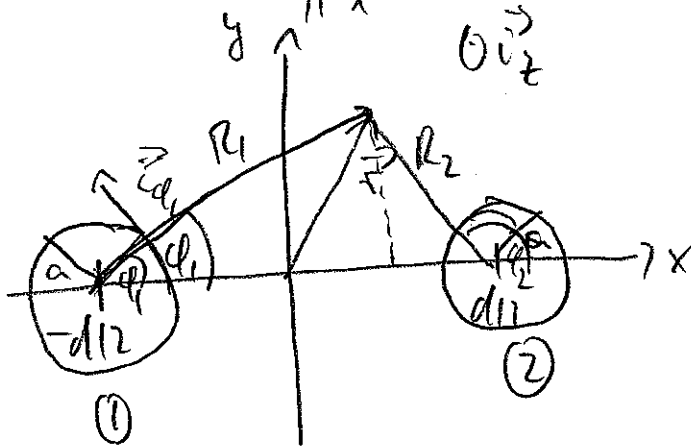
$$\Rightarrow \vec{B}_1 = \frac{\mu_0 i l}{4\pi} \frac{\sqrt{2}}{2} \cdot \frac{4\pi}{l^2} = \frac{\sqrt{2} \mu_0 i l}{2\pi l} \vec{i}_z$$

(4)

Everything else is totally symmetric and gives the same contribution to  $\vec{B}$

$$\Rightarrow \vec{B} = 4\vec{B}_1 = \frac{2\sqrt{2} \mu_0 i}{\pi l} \vec{i}_z$$

(6)



(a)  $\vec{v}$  outside of wires

$$\vec{B}_1 = \frac{i \mu_0}{2\pi R_1} = \frac{i \mu_0}{2\pi R_1} (-\sin \alpha_1 \vec{i}_x + \cos \alpha_1 \vec{i}_y)$$

$$= \frac{i \mu_0}{2\pi R_1} \left( -\frac{y}{R_1} \vec{i}_x + \frac{x + \frac{d}{2}}{R_1} \vec{i}_y \right)$$

$$R_1 = \left[ \left( x + \frac{d}{2} \right)^2 + y^2 \right]^{1/2}$$

$$\vec{B}_2 = \frac{i \mu_0}{2\pi R_2} \left( -\frac{y}{R_2} \vec{i}_x + \frac{x - \frac{d}{2}}{R_2} \vec{i}_y \right)$$

$$R_2 = \left[ \left( x - \frac{d}{2} \right)^2 + y^2 \right]^{1/2}$$



$$\vec{B} = \vec{B}_1 + \vec{B}_2$$

look for  $x, y$  such that  $\vec{B} = 0$

x direction

$$-\frac{y}{R_1^2} - \frac{y}{R_2^2} = 0 \quad \text{Since } R_1, R_2 > 0 \Rightarrow y = 0$$

$\Rightarrow$  y direction

$$\frac{x + \frac{d}{2}}{R_1^2} + \frac{x - \frac{d}{2}}{R_2^2} = 0$$

$$R_1 = \left| x + \frac{d}{2} \right| ; R_2 = \left| x - \frac{d}{2} \right|$$

Cases:

(a)  $x + \frac{d}{2} > 0, x - \frac{d}{2} > 0 \Rightarrow$  no solution

(b)  $x + \frac{d}{2} > 0, x - \frac{d}{2} < 0 \Rightarrow \frac{1}{x + \frac{d}{2}} + \frac{1}{x - \frac{d}{2}} = 0$

$$\Rightarrow x + \frac{d}{2} = -\left(x - \frac{d}{2}\right) \Rightarrow x = 0$$

Since for  $x = 0$  the condition is fulfilled that's a solution (and it's outside the wires too! 😊)

(c)  $x + \frac{d}{2} < 0, x - \frac{d}{2} < 0 \Rightarrow$  no solution either

Only solution outside wires:  $x = y = 0$

(6)

Point on such right wire:

$$\vec{B}_1 = \text{as before}$$

$$\vec{B}_2 = \frac{i\mu_0}{2\pi} \frac{R_2}{a^2} \vec{e}_2$$

$$= \frac{i\mu_0}{2\pi} \frac{R_2}{a^2} \left( -\frac{y}{R_2} \vec{i}_x + \frac{x - \frac{d}{2}}{R_2} \vec{i}_y \right)$$

$$\vec{B}_1 + \vec{B}_2 = 0$$

x-direction

$$-\frac{y}{R_1^2} - \frac{y}{a^2} = 0 \Rightarrow y = 0$$

y-direction

$$\frac{x + \frac{d}{2}}{R_1^2} + \frac{x - \frac{d}{2}}{a^2} = 0$$

Since  $x + \frac{d}{2} > 0$ ;  $R_1 = x + \frac{d}{2}$

$$\frac{1}{x + d/2} + \frac{x - d/2}{a^2} = 0$$

$$a^2 + x^2 - \frac{d^2}{4} = 0 \Rightarrow x = \sqrt{\frac{d^2}{4} - a^2} = \frac{1}{2} \sqrt{d^2 - 4a^2}$$

which is inside the right wire since  $a < \frac{d}{2}$  (2)

Comparison to book: Distance from center of right wire:  $x' = \frac{d}{2} - x$

Solution for point on left wire by symmetry:  $x = -\frac{1}{2} \sqrt{d^2 - 4a^2}$ ,  $y = 0$ .